

equations in a Newtonian central-force field for a circular nominal trajectory. Following Eq. (5) he states that "Eqs. (5) are applicable to perturbations of a general elliptical trajectory. However, the integration to obtain δr and $\delta \theta$ becomes a difficult task because of dependence on time of the unperturbed parameters r and θ ." It will be shown that the solution by elementary functions is possible if the eccentric anomaly E is used as an independent variable. The coordinate system is chosen in such a way that the z axis is perpendicular to the plane of the unperturbed motion. Then, the rigorous differential equation of motion in spatial cylindrical coordinates (r, θ, z) are

$$\ddot{r} + \frac{Kr}{(r^2 + z^2)^{3/2}} - r\dot{\theta}^2 = 0 \quad \frac{d}{dt}(r^2 \dot{\theta}) = 0 \quad (1)$$

and

$$\ddot{z} + \frac{Kz}{(r^2 + z^2)^{3/2}} = 0 \quad (2)$$

The solution corresponding to the nominal initial conditions is called $r = r_0$, $\theta = \theta_0$, $z_0 \equiv 0$ due to the choice of the coordinate system. The solution corresponding to the perturbed initial condition is denoted by

$$r = r_0 + \delta r \quad \theta = \theta_0 + \delta \theta \quad z = \delta z \quad (3)$$

In a straightforward manner, one now could derive equations linear in δr , $\delta \theta$, and δz . But it is immediately clear from the character of Eq. (1) that such a system of differential equations of δr and $\delta \theta$ would be coupled. To avoid this difficulty, the energy integral² is used:

$$\left(\frac{dr}{dt}\right)^2 + r^2 \left(\frac{d\theta}{dt}\right)^2 + \left(\frac{dz}{dt}\right)^2 - \frac{2K}{(r^2 + z^2)^{1/2}} + \frac{K}{a_0} = C_3 \quad (4)$$

where a_0 is the major axis of the unperturbed elliptical motion, K the gravitational constant of the central force field, and C_3 a constant of integration which vanishes if $r = r_0$ and $\theta = \theta_0$. Multiplying the differential equations for r in (1) by r , adding (4), and linearizing yields

$$[d^2(r_0 \delta r)/dt^2] + (K/r_0^3)(r_0 \delta r) = C_3 \quad (5)$$

On the other hand, one obtains by a twofold subtraction of Eq. (5) from the linearized energy integral

$$\frac{d\delta \theta}{dt} = \frac{1}{na_0^2(1-e^2)^{1/2}} \left[\frac{d}{dt} \left(2 \frac{d(r_0 \delta r)}{dt} - \delta r \frac{dr_0}{dt} \right) - \frac{3C_3}{2} \right] \quad (6)$$

Finally, direct linearization of Eq. (2) yields

$$[d^2(\delta z)/dt^2] + (K/r_0^3)\delta z = 0 \quad (7)$$

The integration problem is reduced to the solution of one differential equation of second order, namely

$$(d^2q/dt^2) + (K/r_0^3)q = C \quad (8)$$

With the well-known relation

$$\frac{ndt}{n^2} = \frac{[1 - e \cos(E' + E_0)]dE'}{K/a_0^3} \quad E' = E - E_0 \quad (9)$$

where e is the eccentricity, E the eccentric anomaly, and E_0 the eccentric anomaly corresponding to the beginning of the motion, one derives from the homogeneous part of Eq. (8)

$$[1 - e \cos(E' + E_0)](d^2q/dE'^2) - e \sin(E' + E_0) (dq/dE') + q = 0 \quad (10)$$

A fundamental solution of (10) with the Wronskian equal to one is

$$\begin{aligned} q_1 &= n^{-1/2} [\cos E' - e \cos E_0] \\ q_2 &= n^{-1/2} [\sin E' + e \sin E_0] \end{aligned} \quad (11)$$

Thus, the general solution of (8) can be written as

$$q = C_1 q_1 + C_2 q_2 + C \left\{ q_2 \int_0^{E'} q_1 dt - q_1 \int_0^{E'} q_2 dt \right\} \quad (12)$$

$$E' = E - E_0$$

From Eqs. (9) and (11) it follows that the integrals in (12) can be expressed as trigonometric functions of E and rational functions of e . For the sake of brevity, the explicit expressions are not written down, but it might be pointed out that the six constants of integration can be determined independently from each other if the quantity $E' = E - E_0$ is introduced. This follows easily from the character of Eqs. (6, 7, and 12). For an application of this classical method in perturbed central force fields, see Ref. 3.

References

- 1 Wisneski, M. L., "Error matrix for a flight on a circular orbit," *ARS J.* **32**, 1416-1418 (1962).
- 2 Brouwer, D. and Clemenc, G. M., *Methods of Celestial Mechanics* (Academic Press, New York and London, 1961).
- 3 Dusek, H. M., "Theory of error propagation in astro-inertial guidance systems for low-thrust earth orbital missions," *ARS Preprint* 2683-62 (November 1962).

Reply to Comment by H. M. Dusek

M. L. WISNESKI*

The Boeing Company, Seattle, Wash.

THE comment of Mr. Dusek and his ARS meeting paper are very interesting. It appears that a manageable solution of Eqs. (5) of his Ref. 1 can be obtained if the technique of his Ref. 2 for dealing with such equations is employed. The technique uses eccentric anomaly as an independent variable. However, to express perturbations in terms of the true anomaly rather than the eccentric anomaly, the conversion involves a series expansion. Thus an additional approximation, strictly valid for low-eccentricity orbits, has to be made when only the first few terms are retained.

In Dusek's Ref. 1 signs in two places are incorrect. Referring to the last two "error matrices," the signs in front of expressions in positions 2 and 3 should be plus.

Received by ARS November 26, 1962.

* Research Engineer, Physics Technology Department, Aero-Space Division.

Response to Author's Reply

HERMANN M. DUSEK*

General Motors Corporation, El Segundo, Calif.

THE introduction of the true anomaly is pertinent neither to my original comment nor to Wisneski's original paper. Wisneski states, "However, to express perturbations in terms of the true anomaly rather than the eccentric anomaly, the conversion involves a series expansion." This statement, in itself, certainly is true if one follows the classical astronomical practice (see Ref. 2, pp. 62-65, of the original comment). However, to this author's knowledge, series expansions for arbitrary eccentricities of the unperturbed orbit in connection with this particular problem can be avoided.

Received March 28, 1963.

* Head, Space Studies, AC Spark Plug Division. Member AIAA.